

GLASS PERFORMANCE DAYS 2025

Structural optimisation of glass plates

Motivation

Architectural Glass



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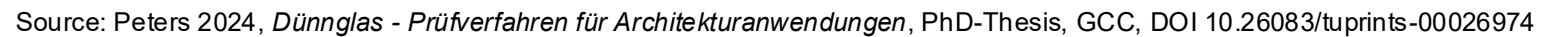


Music hall (Muis Sacrum Arnhem)



Vakko Headquarter (Source: Knaack, 2010)

Architectural Glass – Flat glass (EN 572-2 thickness range 2...25 mm)



Motivation

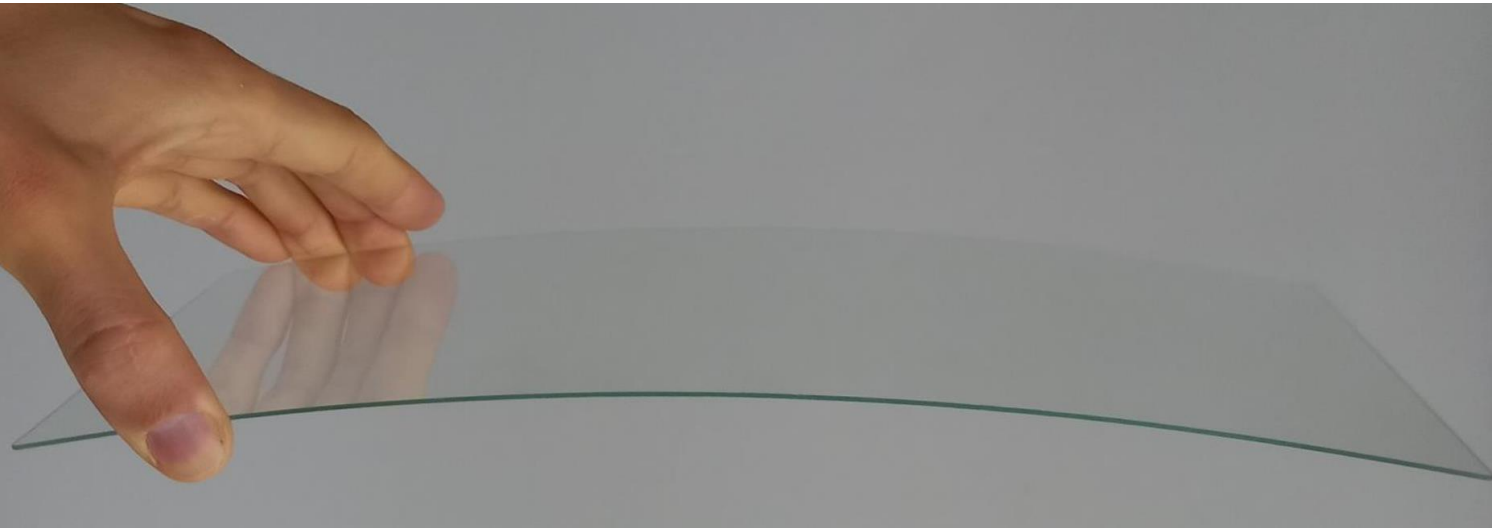
Architectural Glass



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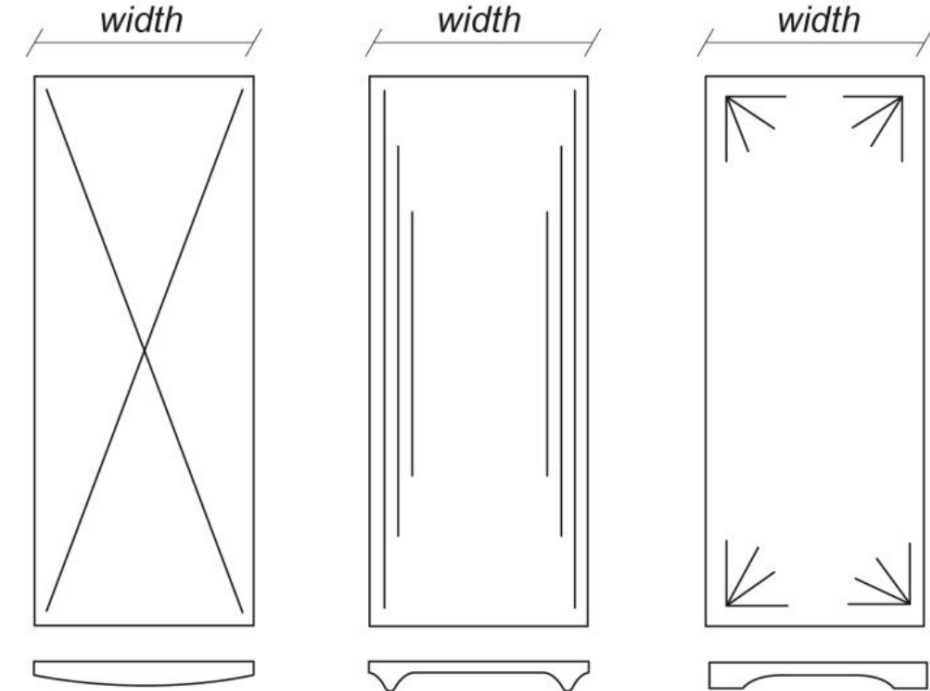


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SLS is the limiting factor ($L/100$)

1 kg flat glass $\approx$ 1 kg CO₂ equ. (GWP)



Source: Seel et al 2018 *Fused glass deposition modelling for applications in the built environment*. <https://doi.org/10.1002/mawe.201800075>

Structural optimisation – Types

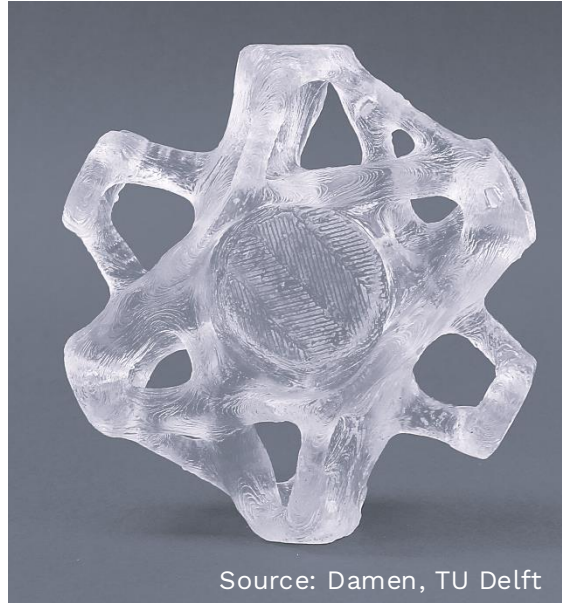


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Topology optimisation



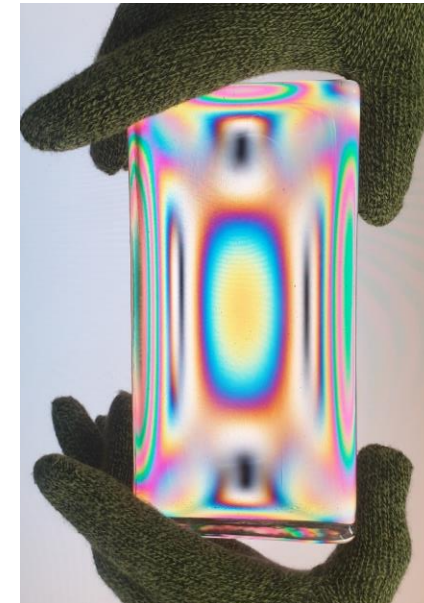
Shape optimisation



Topography optimisation



Material optimisation



Visualisation

Stiffness (max)
Mass (min)

σ (min)
 $d\sigma'/dx_i$ (min)

I_y (max)
Mass (min)

f_k (max)
 $E_{\parallel}; E_{\perp}$

Target
values

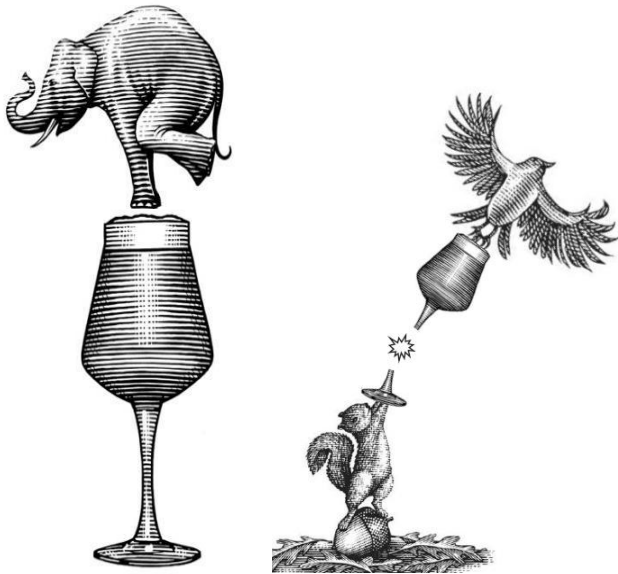
Structural optimisation – Constrains



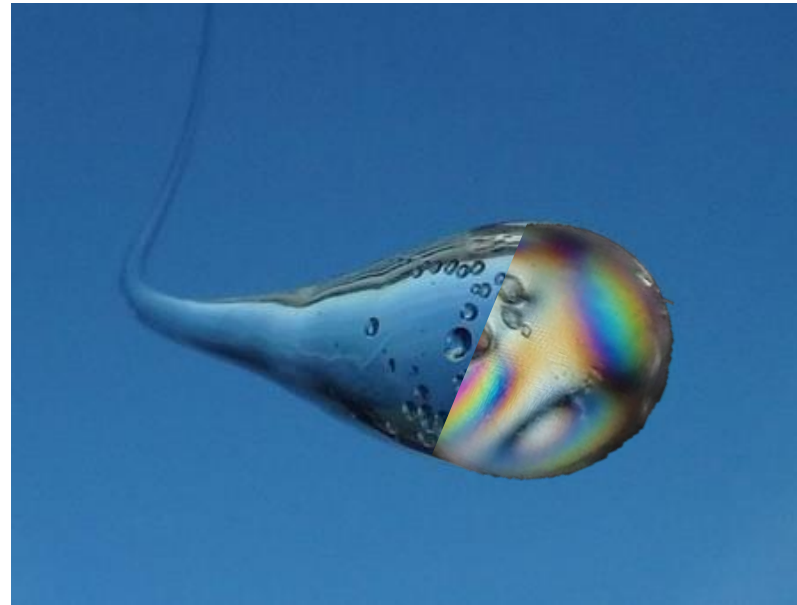
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Source: Images from Steven Noble



Source: <https://eu.metrowestdailynews.com>

Structural optimisation – Manufacturing

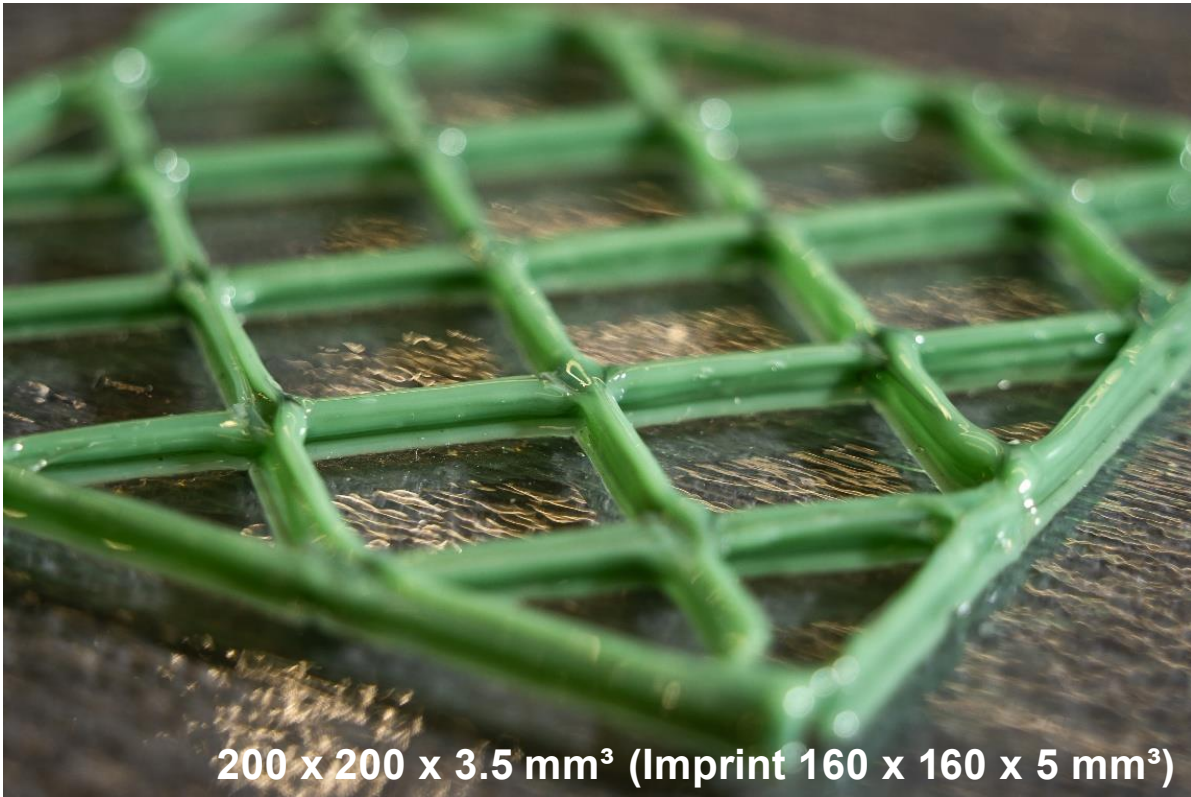
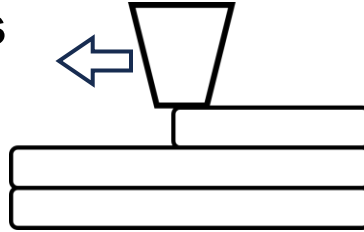


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Additive Manufacturing of Glass



200 x 200 x 3.5 mm³ (Imprint 160 x 160 x 5 mm³)

Source: MapleGlass + GCC

Glass shaping for lowering areas



Source: GLAPE/IWM + GCC

Structural optimisation – Topology

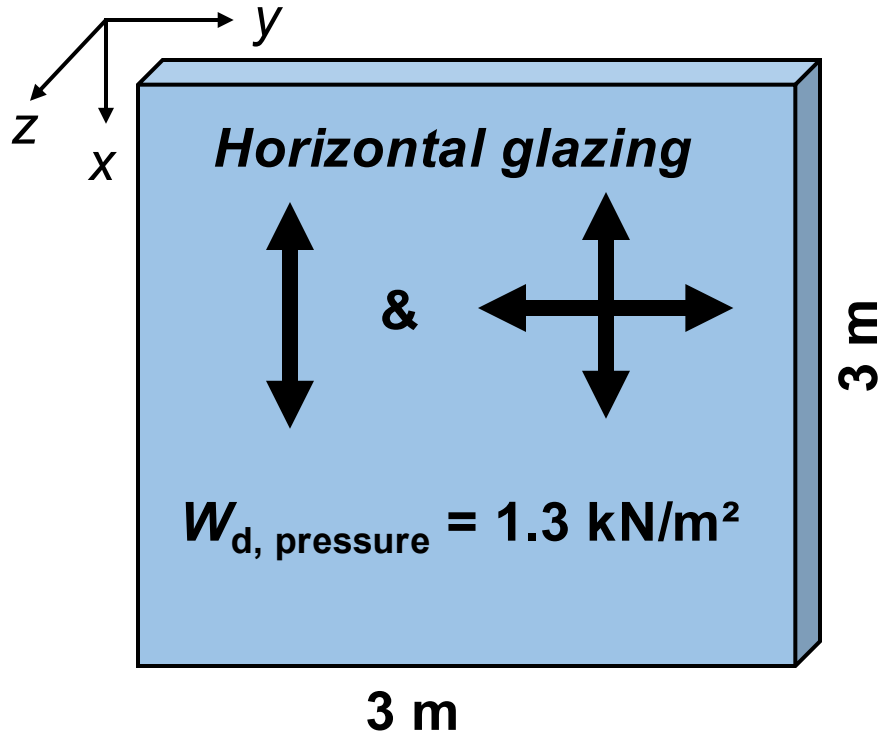


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Task



Model assumptions and boundary conditions

- Min./max. construction height of 10 / 200 mm (glass cross-section)
- Min. glass thickness of flat glass 4 mm,
- Design wind load w_d amounts 1.3 kN/m^2 (pressure),
- 2-sided or 4-sided linear (Navier) support
- Stiffening geometry without overhang (angle = 0°),
- Minimisation of contact surface between base plate and the imprint for optical reasons
- Calculation of optimisation with geometrically linear method

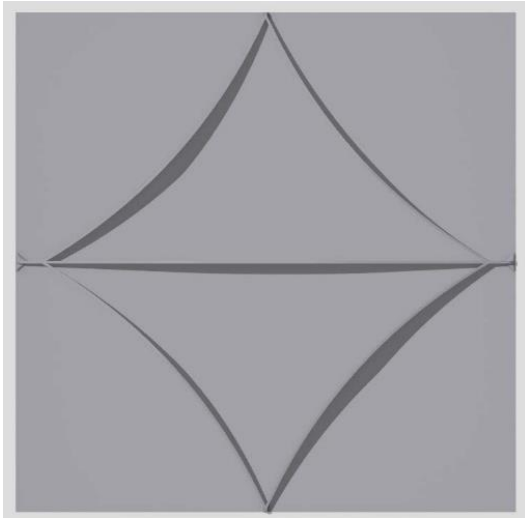
Design limit value according DIN 18008 (Constraints)

- $C_d = L/100 = 30 \text{ mm}$ (SLS – criteria)
- $f_{y,d} = 17 \text{ MPa}$ (ULS – criteria, annealed glass)

Structural optimisation – Topology

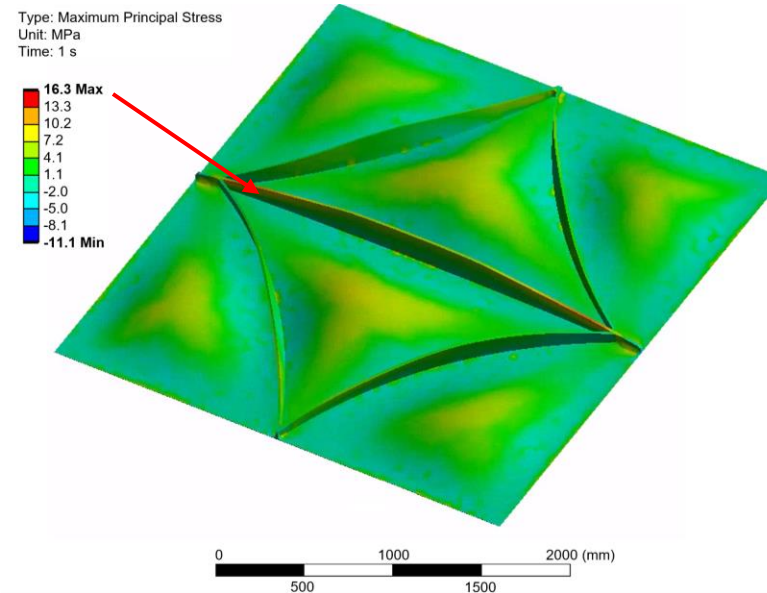
Results – 4 sided-support (4-ops1)

Topology optimisation



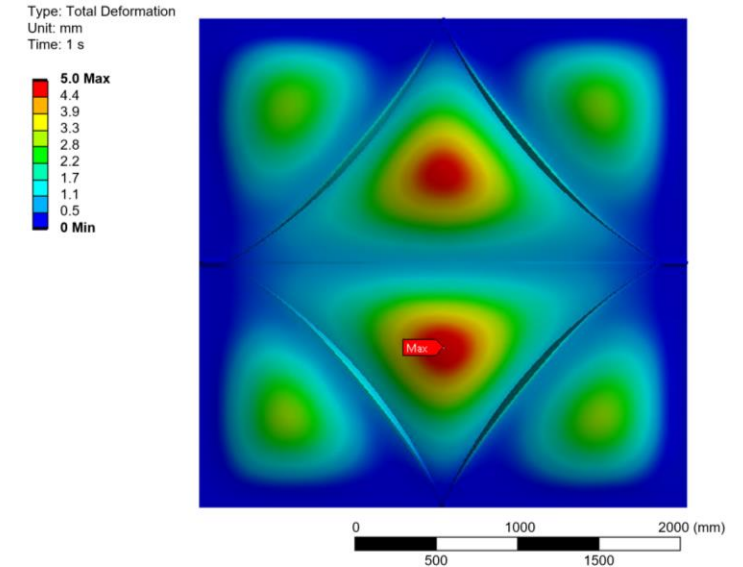
4 mm flat glass + imprint
196 mm
Mass 140 kg

Stress analysis



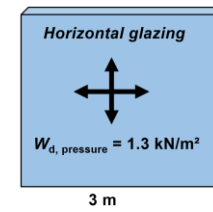
Max. stress 16 MPa

Deformation analysis



Max. deformation 5 mm

59% less mass than reference plate (thickness 15 mm)



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Structural optimisation – Topology

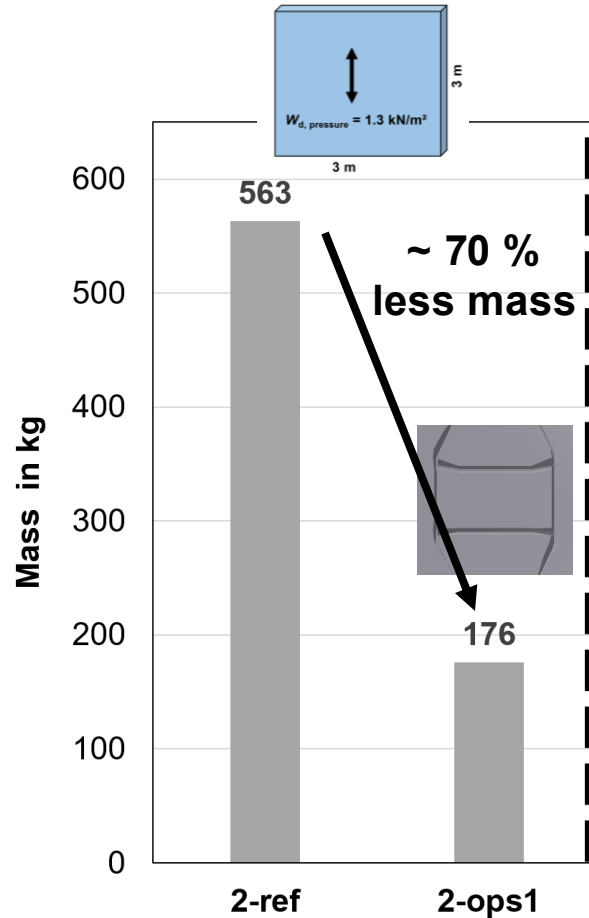


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Results – overview



Variant of structural optimisation

Criteria / Variants	2-ref	2-ops1
Type of support	2-sided	2-sided
Glass built up	25 mm glass plate	4 mm glass plate +196 mm imprint

**SLS is not relevant →
ULS is limiting factor + (stability)**

Max. deflection [mm]	25.9	7.3
Mass [kg]	563	176 (= 90 + 86)
Mass reduction (base ref.) [%]	-	69
Limitation criteria	ULS/SLS	ULS

Notes: * ... Result based on geometrically non-linear calculation

** ... Comparison with result of geometrically non-linear calculation of reference (4-sided)

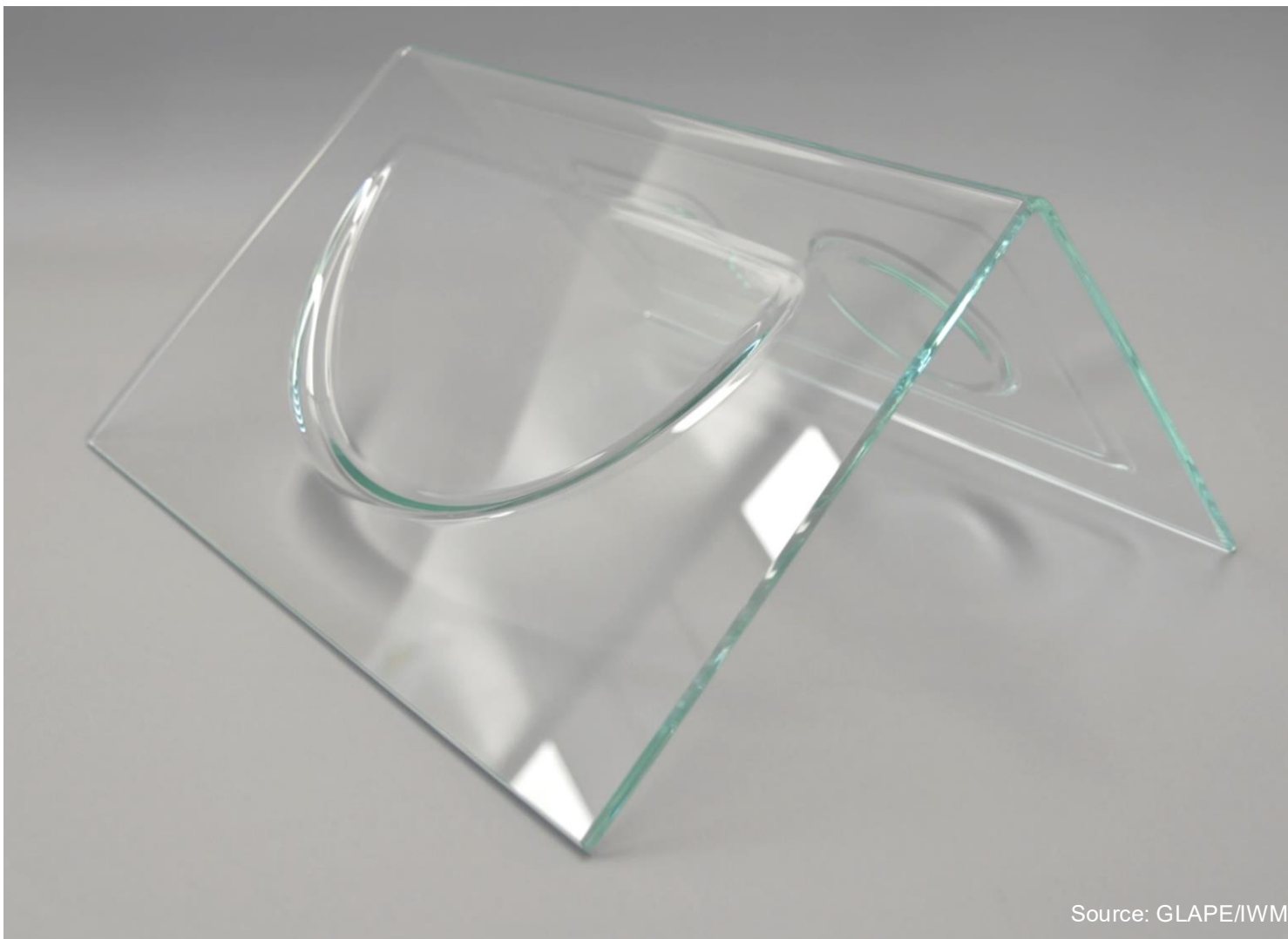
Structural optimisation – Topography



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Source: GLAPE/IWM

Structural optimisation – Topography



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3 lowering areas/beads each 40 mm width over 500 mm (B)

Cross-section (Dimensions in mm)

Cross-section: CS 2-0: 2 mm thick flat glass; 0 mm lowered beads; Area of cross-section 1000 mm²; Moment of inertia 333 mm⁴

Cross-section: CS 2-2: 2 mm thick flat glass; 2 mm lowered beads; Area of cross-section 1000 mm²; Moment of inertia 1142 mm⁴

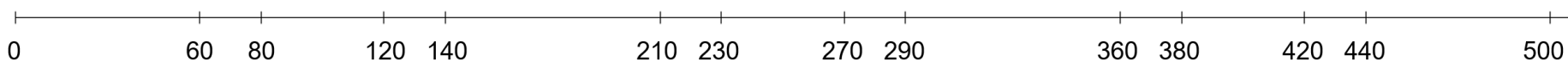
Cross-section: CS 2-4: 2 mm thick flat glass; 4 mm lowered beads; Area of cross-section 1000 mm²; Moment of inertia 3571 mm⁴

Cross-section: CS 4-0: 4 mm thick flat glass; 0 mm lowered beads; Area of cross-section 2000 mm²; Moment of inertia 2666 mm⁴

Cross-section: CS 4-4: 4 mm thick flat glass; 4 mm lowered beads; Area of cross-section 2000 mm²; Moment of inertia 9143 mm⁴

Cross-section: CS 4-8: 4 mm thick flat glass; 8 mm lowered beads; Area of cross-section 2000 mm²; Moment of inertia 28573 mm⁴

Cross-section: CS 8-0: 8 mm thick flat glass; 0 mm lowered beads; Area of cross-section 4000 mm²; Moment of inertia 21333 mm⁴



Legend

 Areas of lowering



Structural optimisation – Topography



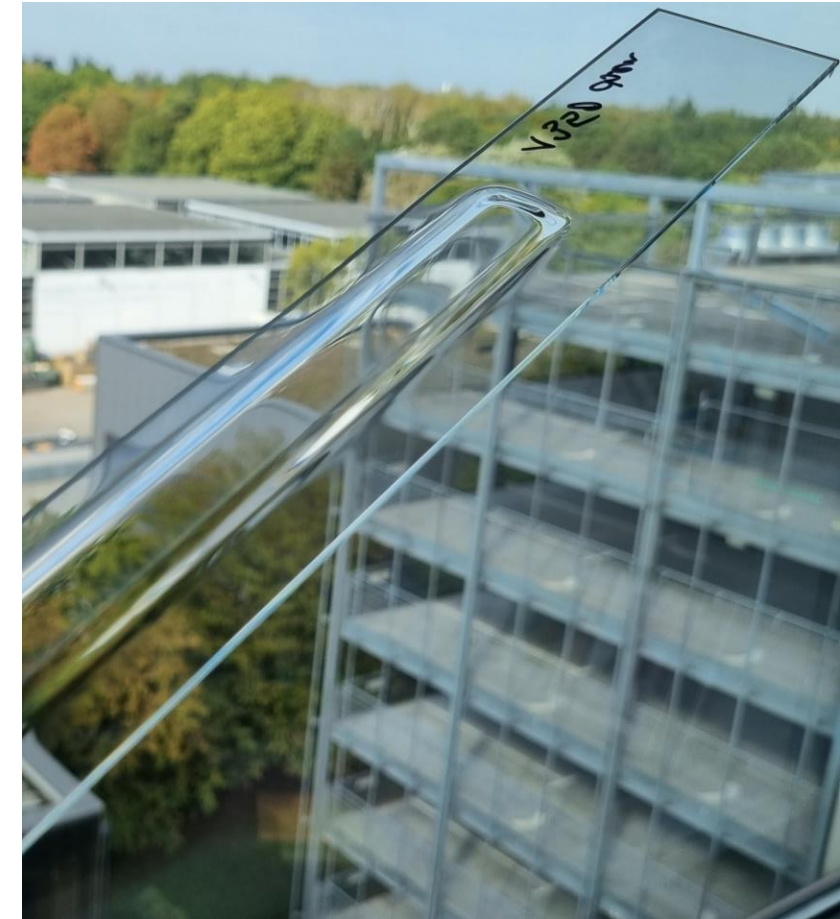
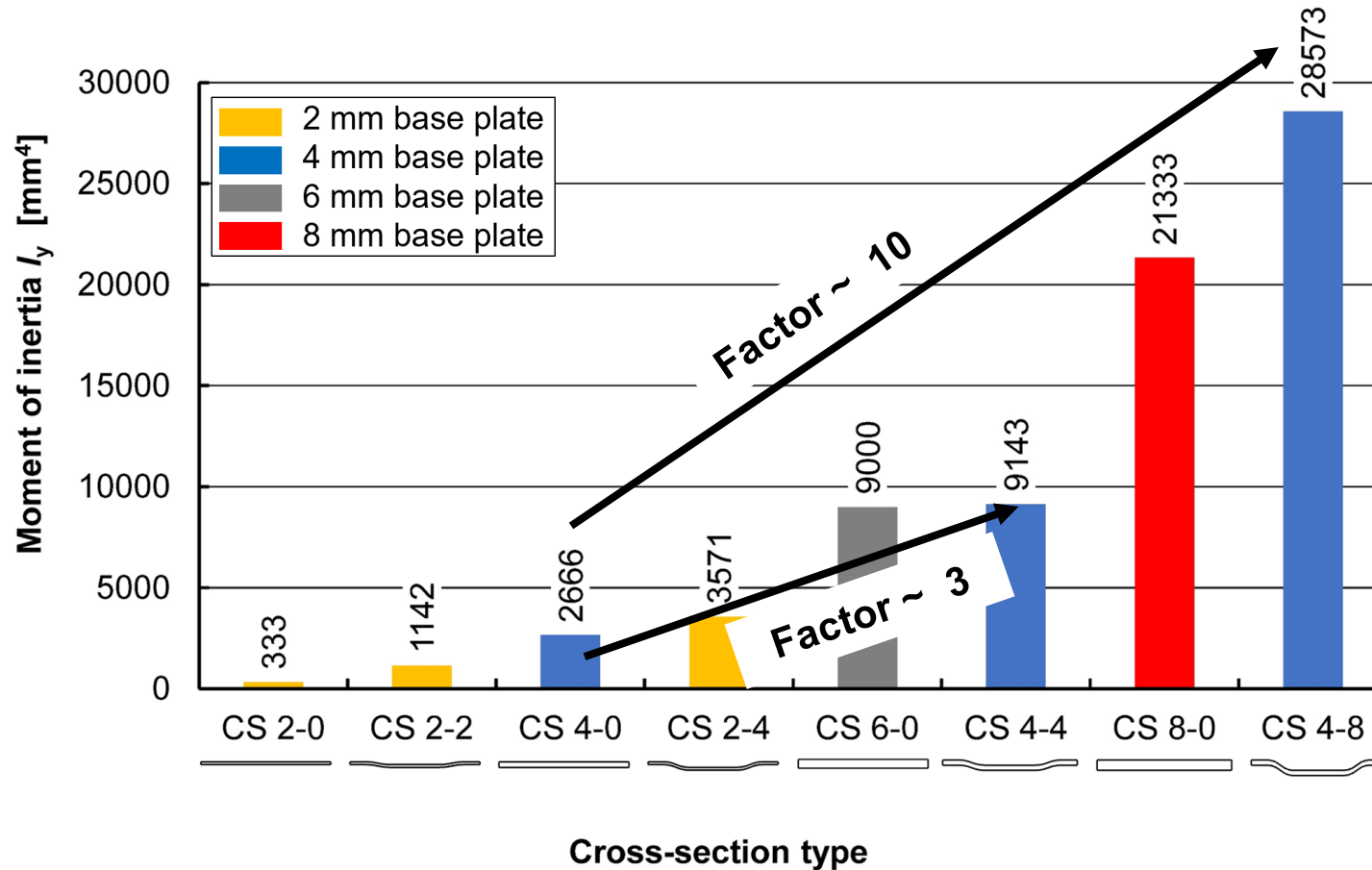
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3 lowering areas/beads each 40 mm width over 500 mm (B) – results

Cross-section (Dimensions in mm)



Structural optimisation – Topography



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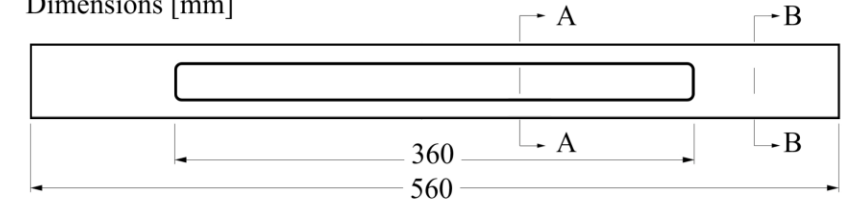
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Experimental results (3 x 50 x 560 mm³)

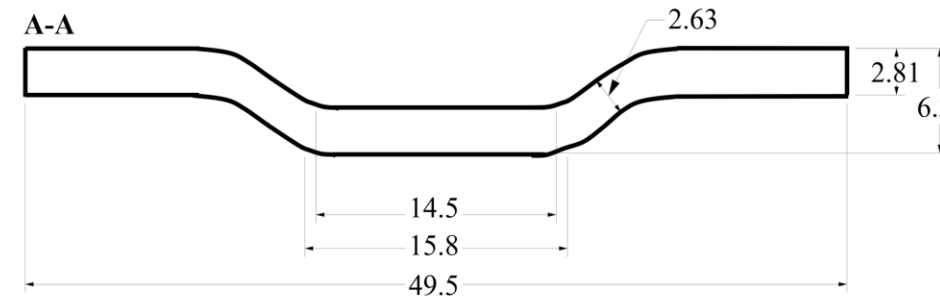


Top view

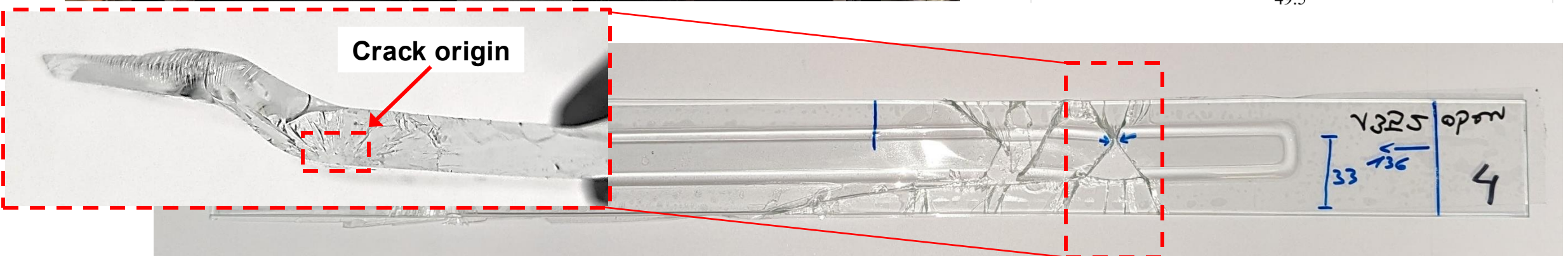
Dimensions [mm]



A-A



Crack origin



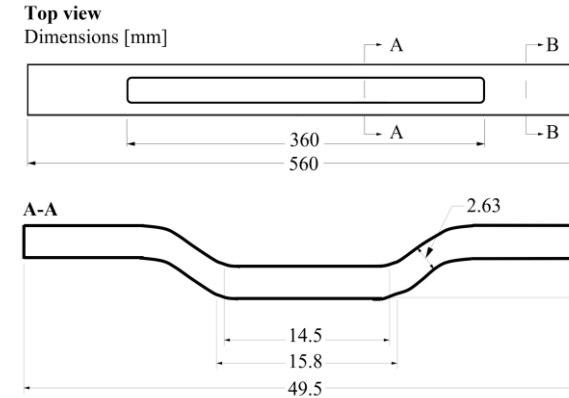
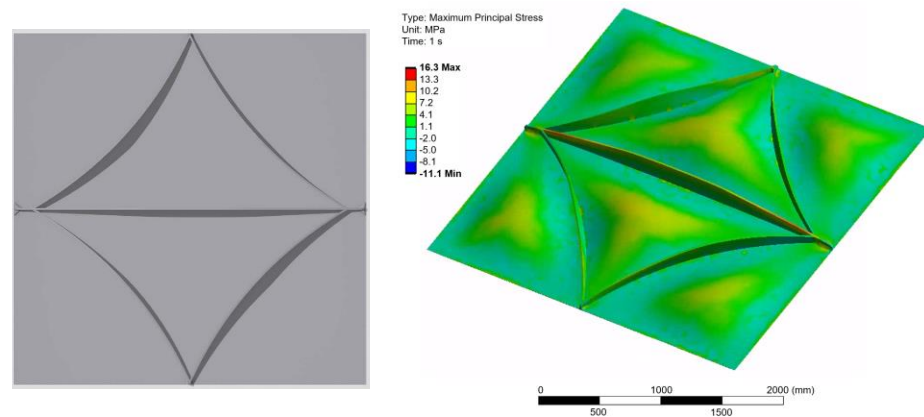
Conclusion



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Structural optimisation for 3D,
but not for 2.1 D
("no software")

Manufacturing techniques "3D
glass printing" / "local forming" is
state of the scientific research

Structural optimisation
→ **Lightweight @ glass structures**
→ **Significant weight reduction**

→ **Architectural benefits**

UpScaling to facade size
is essential

Safety aspects
(laminations & pre-stressing?)

SLS is not relevant →
ULS is limiting factor + (stability)

Outlook

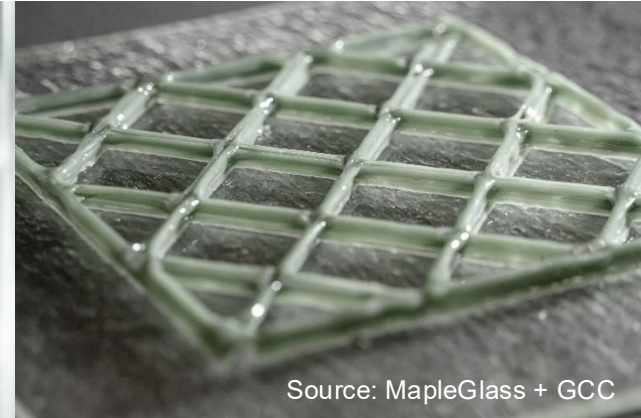


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Vision of stiffened glass structures in architecture



Source: MapleGlass + GCC

Source: Nowak, GCC

Outlook

Vision of non-flat glass in architecture



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Source: GLAPE/IWM

Source: Nowak, GCC

Outlook

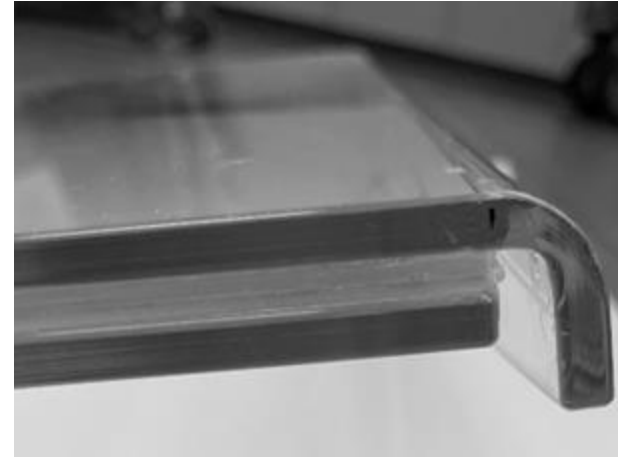
“Vision” of stiffened stair treads



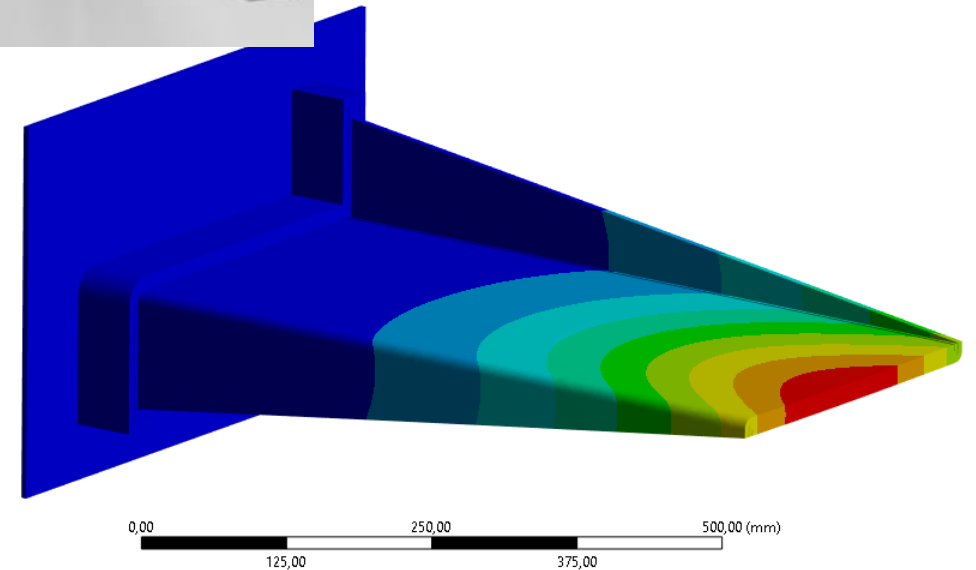
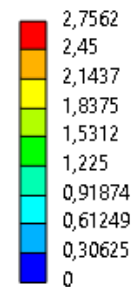
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E: perfekter Verbund
Total Deformation
Type: Total Deformation
Unit: mm
Time: 1 s
Max: 2,7562
Min: 0
28.06.2024 15:26



Source: HB Fuller + GLAPE/IWM + Yachtglas + + Hölscher + Glas Lippold + EOC + GCC

**Thank you
for
your
attention**



Contact:

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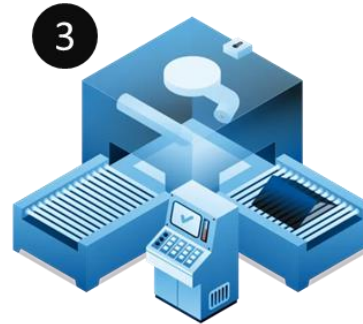
Glass shaping for lowering areas



Heating

Laser induced bending
process

Cooling



Source: GLAPE/IWM + GCC