

GLASS PERFORMANCE DAYS 2025

Multi-Material Polymeric Interlayers

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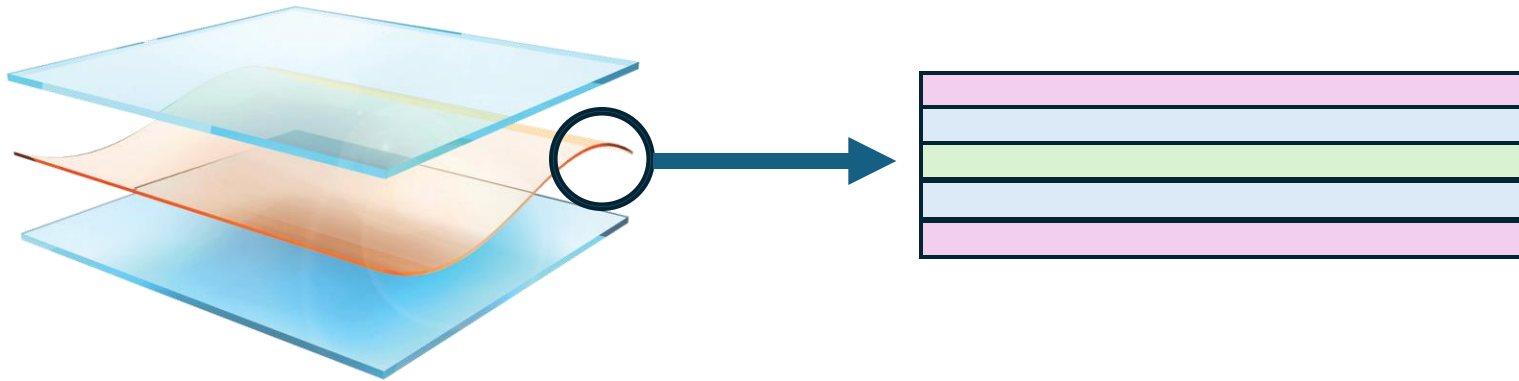
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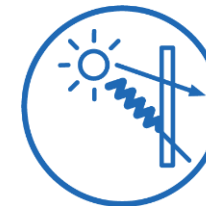
Multi-Material Polymeric Interlayer



Interlayer composed of different materials

Enhances some characteristic of the full stack:

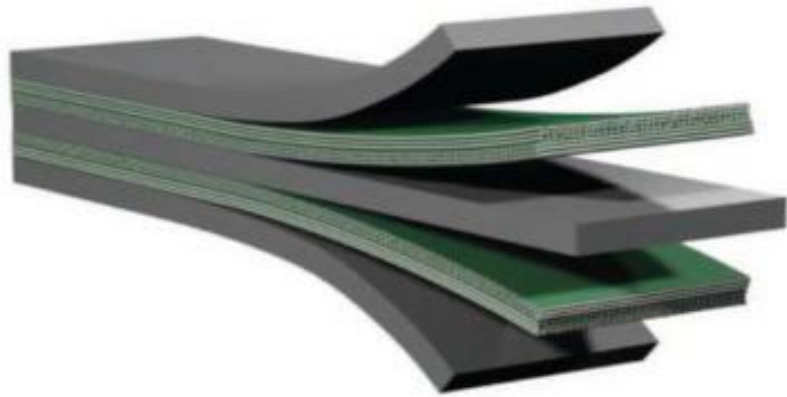
- ✓ Acoustic insulation performance -> Damping
- ✓ Optical transmissivity
- ✓ Mechanical strength
- ✓ Electrical connectivity (PDLC)



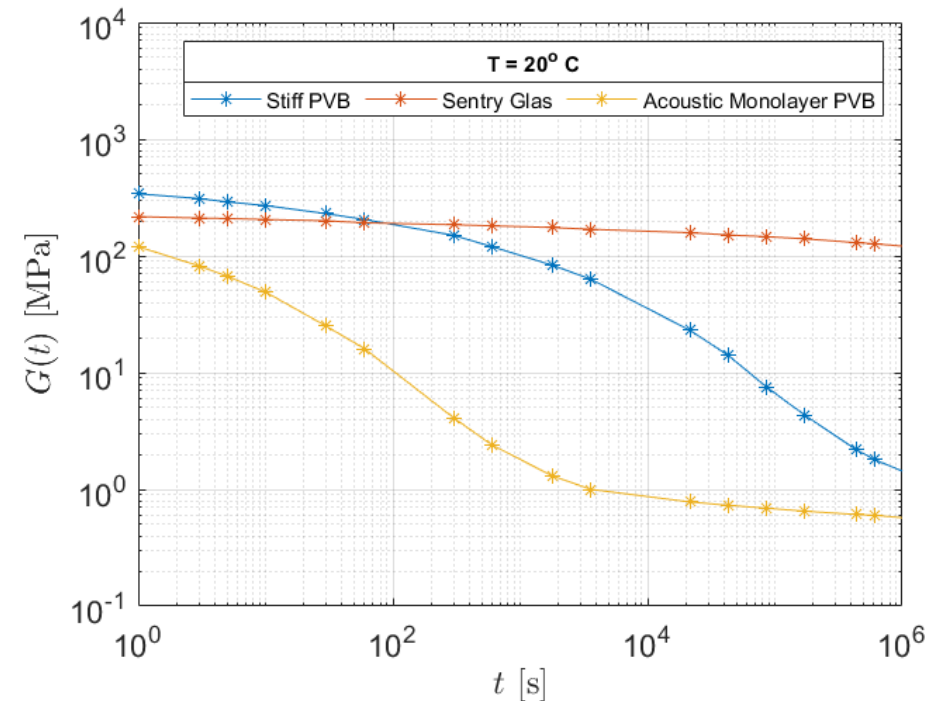
Multi-Material Polymeric Interlayer

Each material has its own:

- **Relaxation function**
- **Thickness**

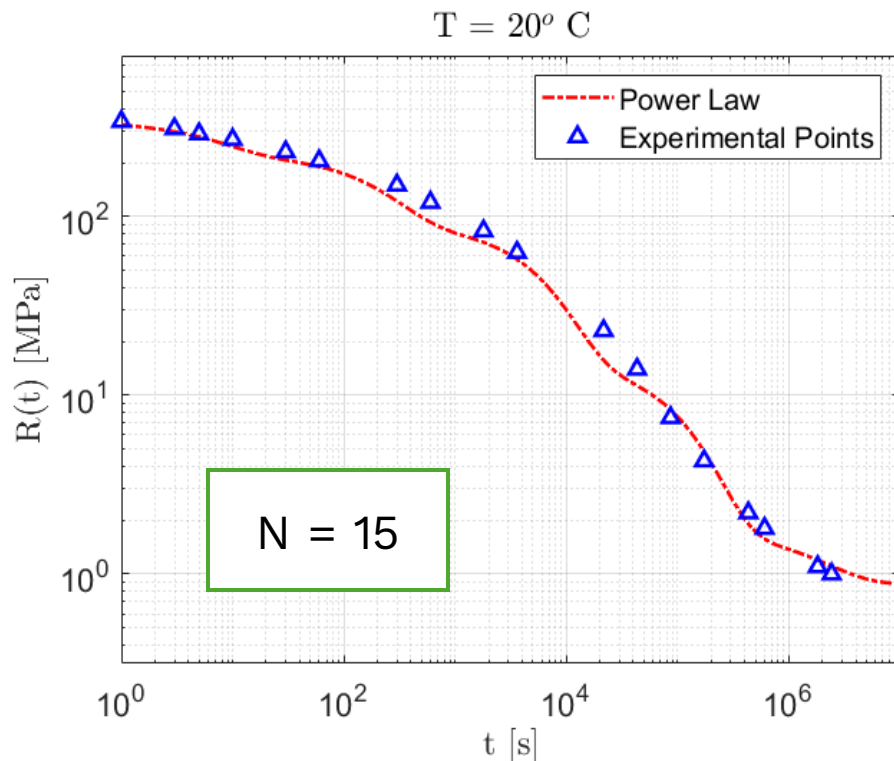


Difficulty in modelling
mechanical properties of the
laminated package



Relaxation function of the polymeric interlayer: ***Prony Series approximation***

$$R(t) = R_0 + \sum_{i=1}^N R_i e^{-t/\vartheta_i}$$



where:

R_i : i-th relaxation shear modulus

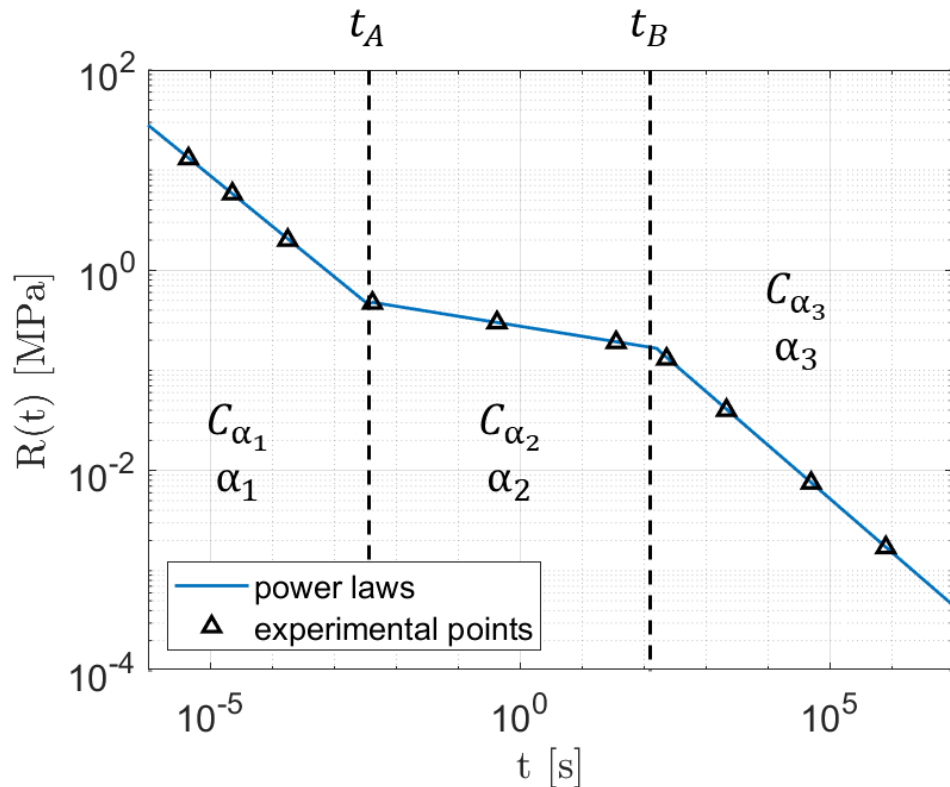
ϑ_i : corresponding relaxation time.

R_0 : material stiffness at t=0.

- G(t) is described by a **Prony series**
- An algorithm is necessary to calibrate the parameters
- Calibration not straightforward

Relaxation function of the polymeric interlayer: **Power law approximation**

$$G(t) = \frac{C_\alpha}{\Gamma(1 - \alpha)} t^{-\alpha}$$

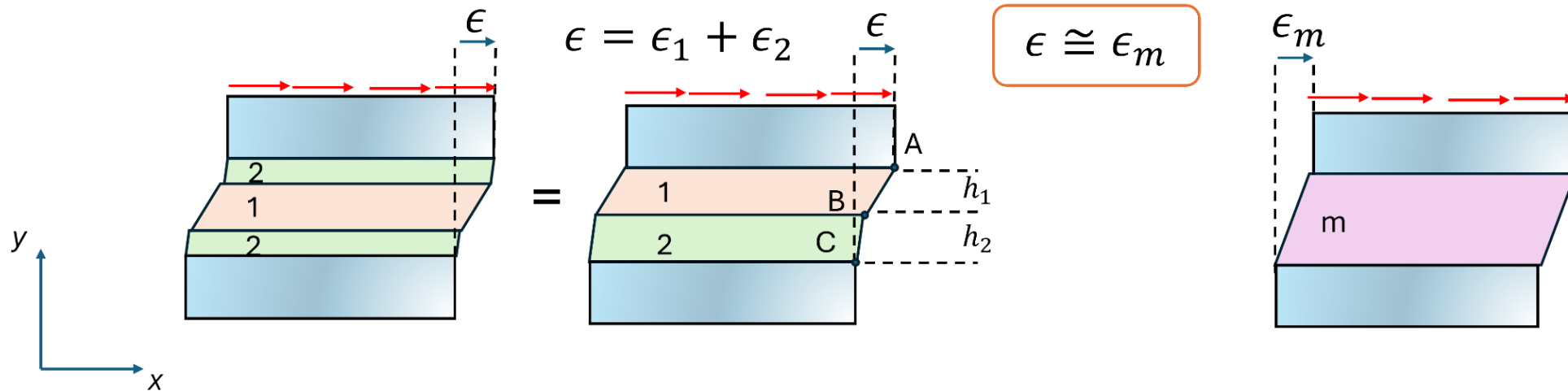


- In the bi-log plot they are **lines**
- α the slope of the line, with $0 < \alpha < 1$
- $C_\alpha [MPa s^\alpha]$ is the stiffness value at $t = 1 s$.

- ✓ The whole $G(t)$ can be approximated by connected branches of **power laws**
- ✓ Geometric interpretation of the parameters
- ✓ Straightforward calibration

The model

- Simplest case: pure shear applied to the stack,
- The total deformation is the sum of the deformations of the interlayer materials,
- One can calculate the total relaxation function once the relaxation function of the various interlayer materials is known.



The model scheme

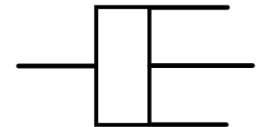
- **In elastic solids:** stress is proportional to the zero-order derivative of strain.



$$\tau(z, t) = K[\epsilon(z, t)]$$

- **In liquids:** stress is proportional to the first derivative of strain.

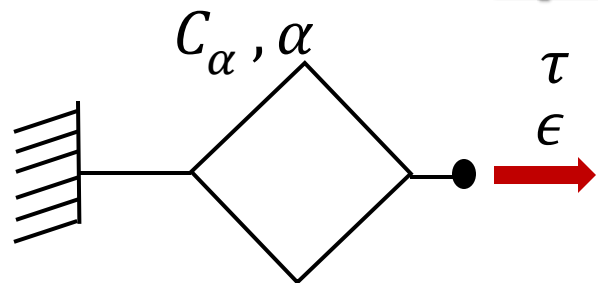
Dashpot



$$\tau(z, t) = \mu \frac{\delta}{\delta t} [\epsilon(z, t)]$$

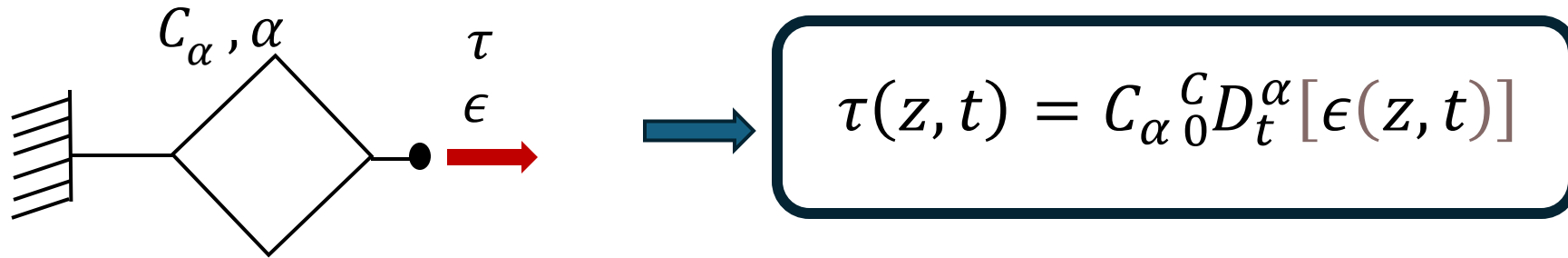
- **Viscoelastic materials:** stress is proportional to a real-order derivative, intermediate between 0 and 1 of the strain over time.

Spring Pot



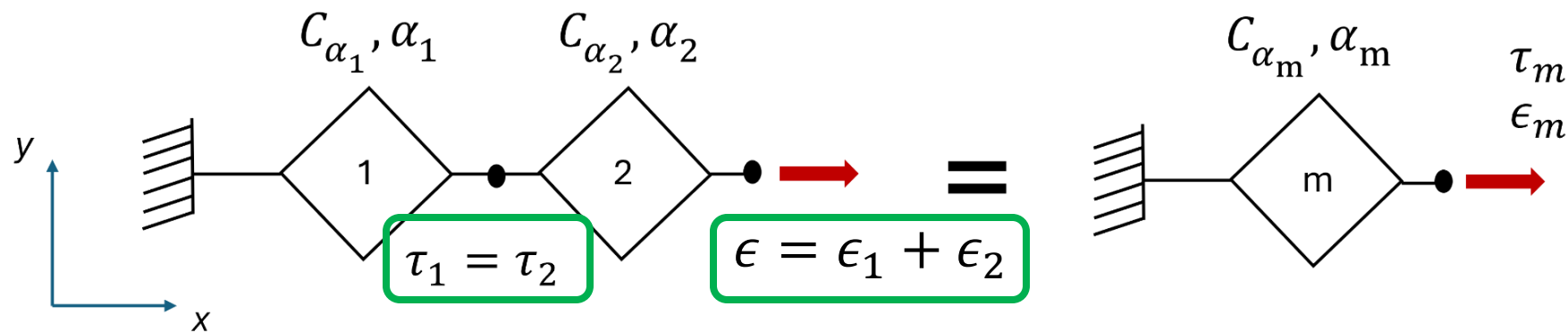
$$\tau(z, t) = C_{\alpha} {}^C D_t^{\alpha} [\epsilon(z, t)]$$

The model scheme



Laminated package with MMPI is modeled with **Spring-Pots in series**:

- the total displacement is the **sum** of the **element displacements**,
- **Same stress** in every element

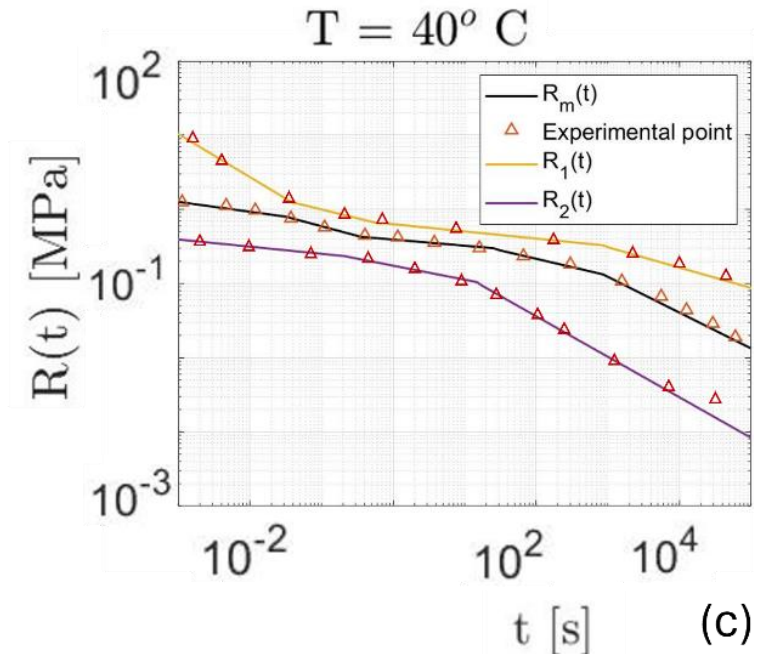
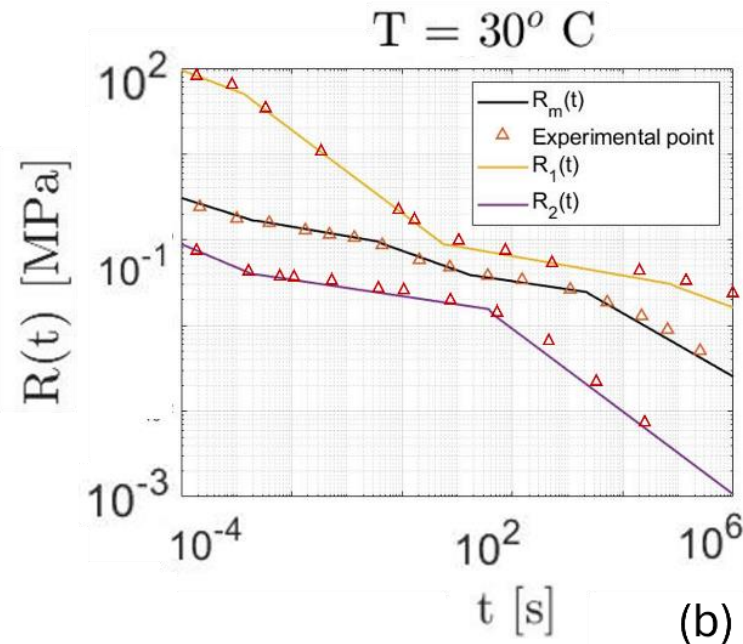
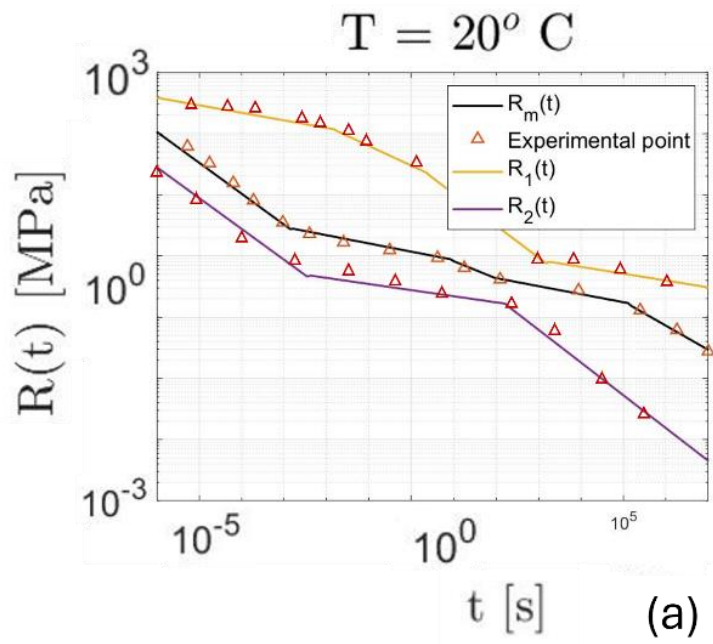


Relaxation functions from DMTA (Dynamic Thermal Material Analyzer)

R_1 = Stiff PVB

R_2 = Acoustic Monolayer PVB (Trosifol Sound Control Monolayer)

R_m = Combination of the two materials



The FE model

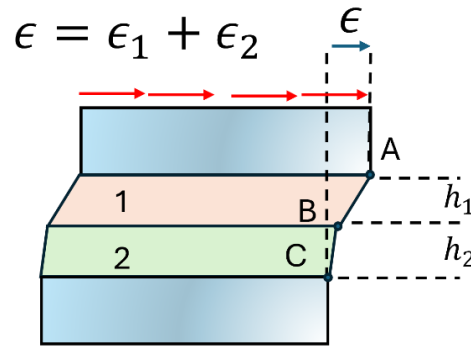


From the Relaxation Functions of DTMA:

- 1) Outer Layer
- 2) Inner Layer



Calculate the total deformation ϵ



Calculate the total shear stress τ

By reversing the constitutive equation of the polymeric

$$\tau(z, t) = \tau(z, 0)R(t) + \int_0^t \frac{\partial \epsilon}{\partial \bar{t}} R(t - \bar{t}) d\bar{t}$$

FULL VISCOELASTIC ANALYSIS



Calculate the Relaxation function of the Multilayer

$R(t)$

Concept of the model

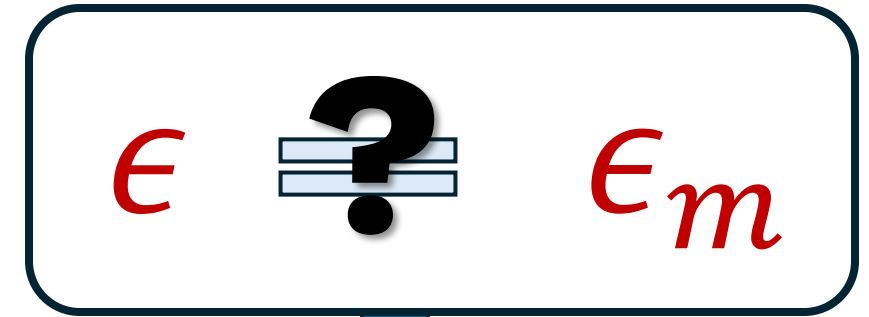
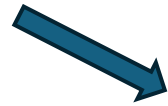
**Relaxation
function DTMA:**

1) Outer Layer

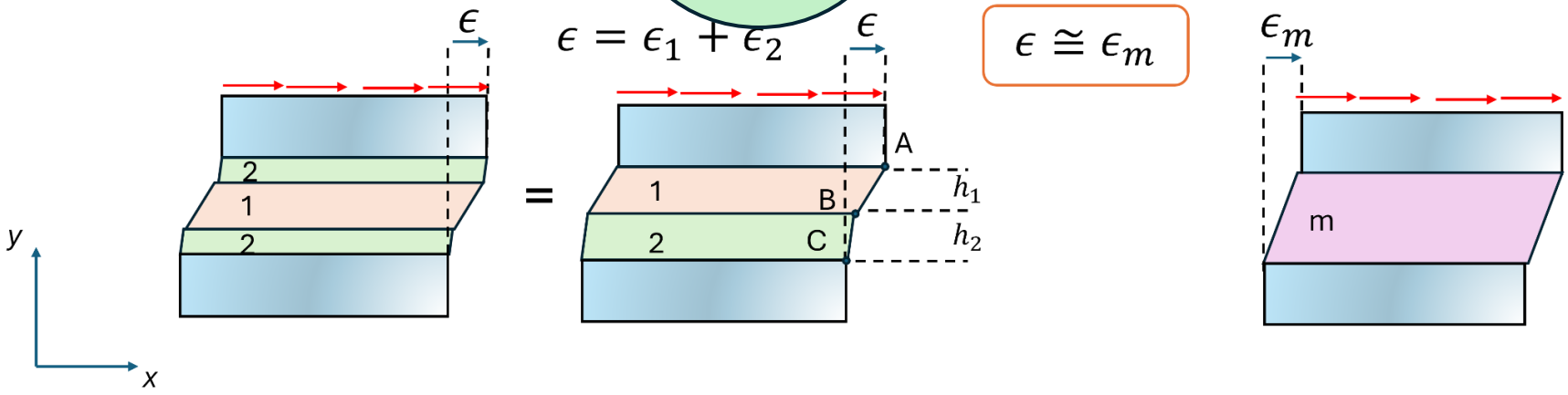
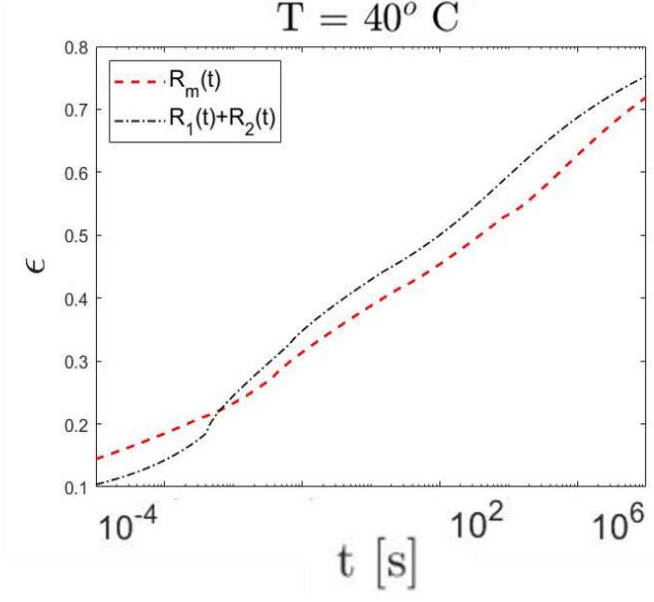
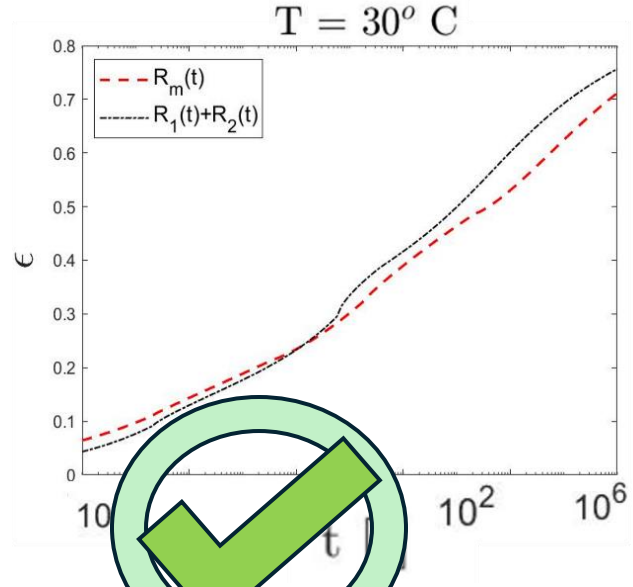
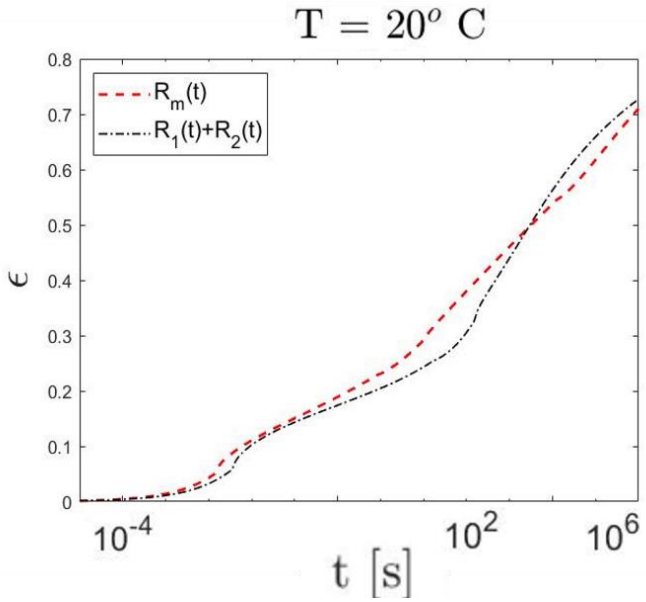
2) Inner Layer

**Relaxation
function DTMA:**

Multi-Material



Model Results: Deformation Comparison

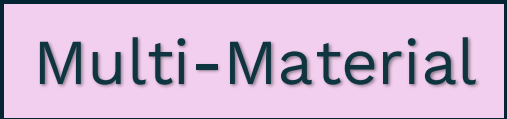


Concept of the model

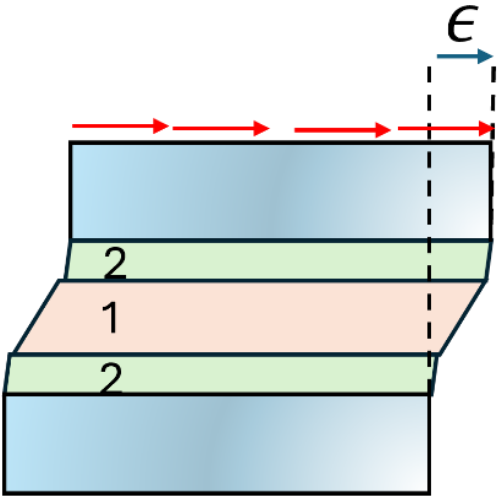
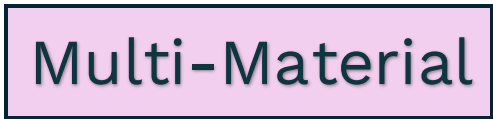
Relaxation function DTMA:



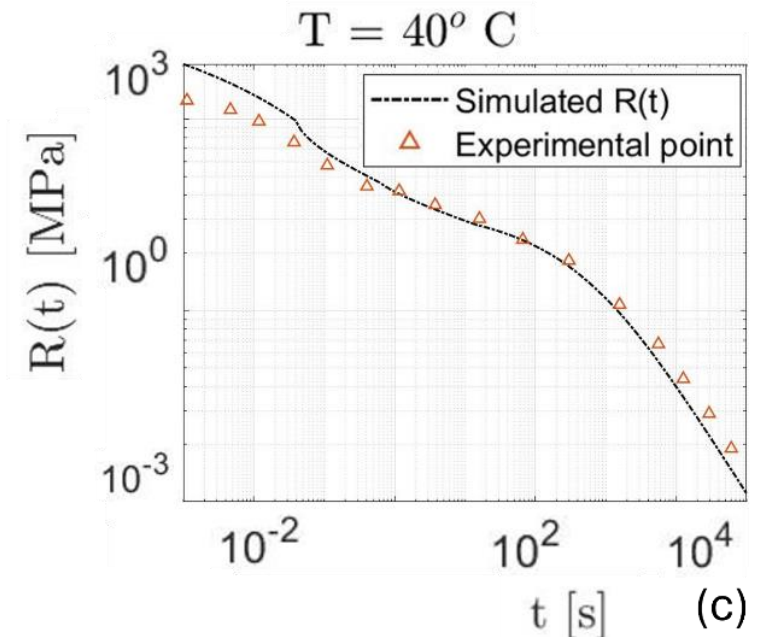
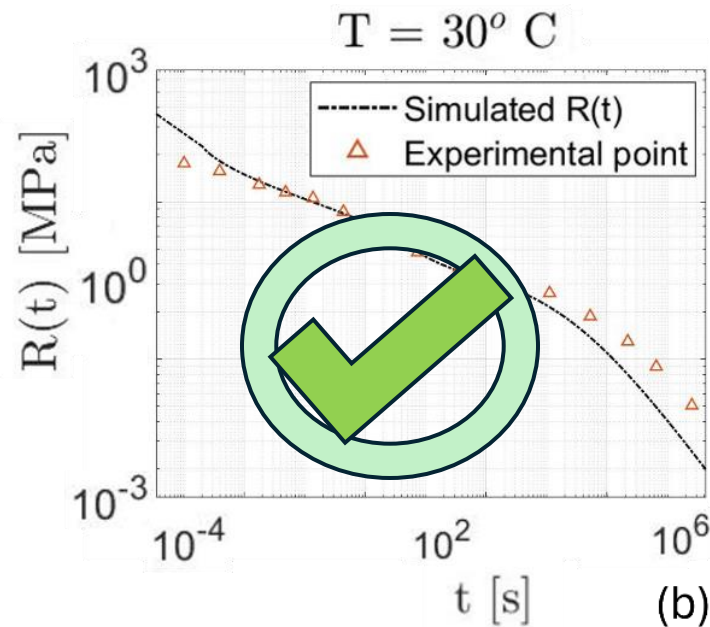
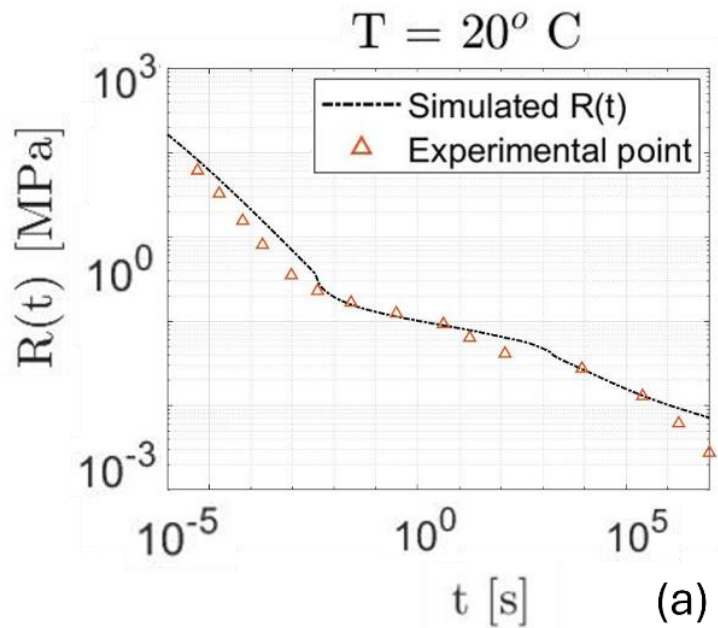
Simulated



Relaxation function DTMA:



Model Results: Simulated vs Experimental Relaxation Function

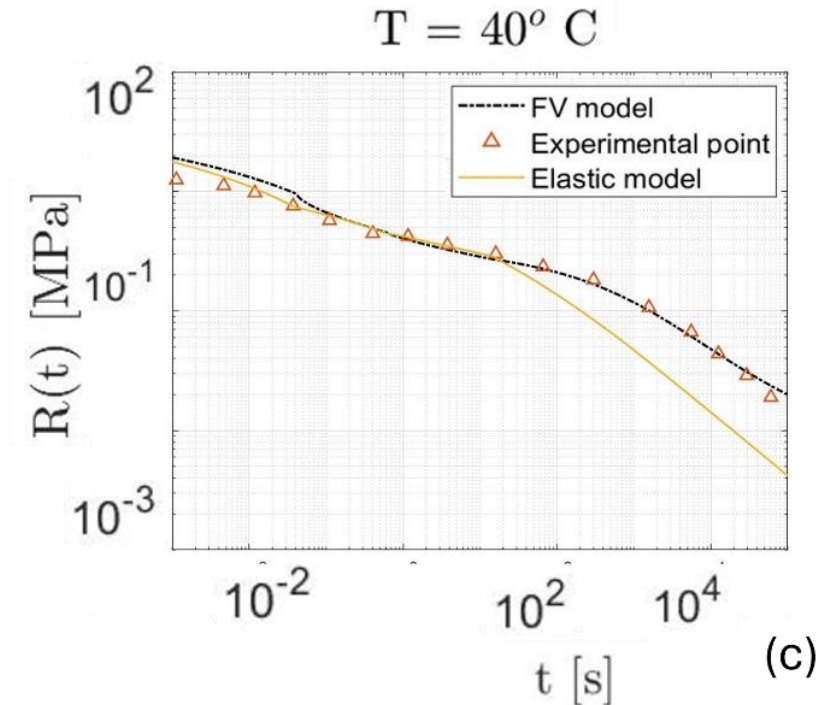
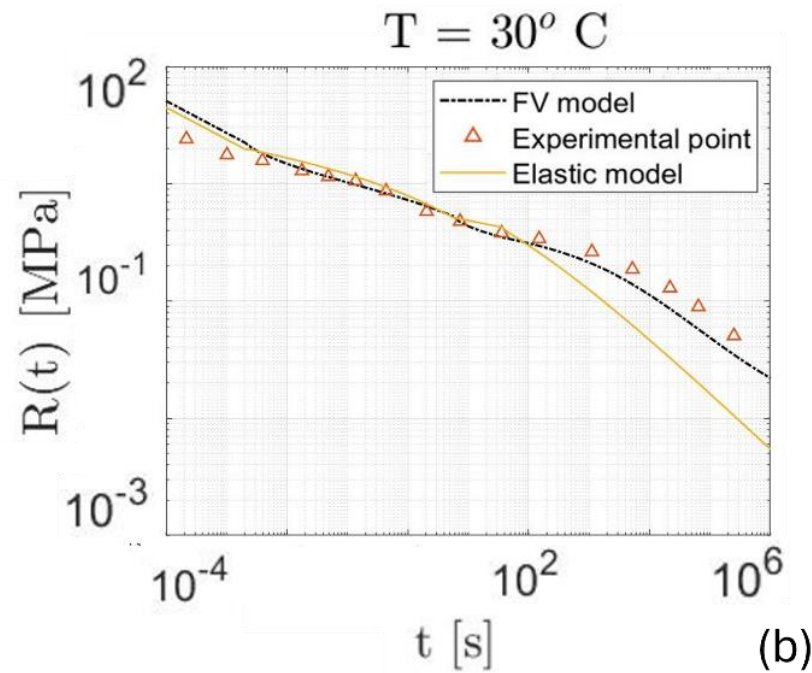
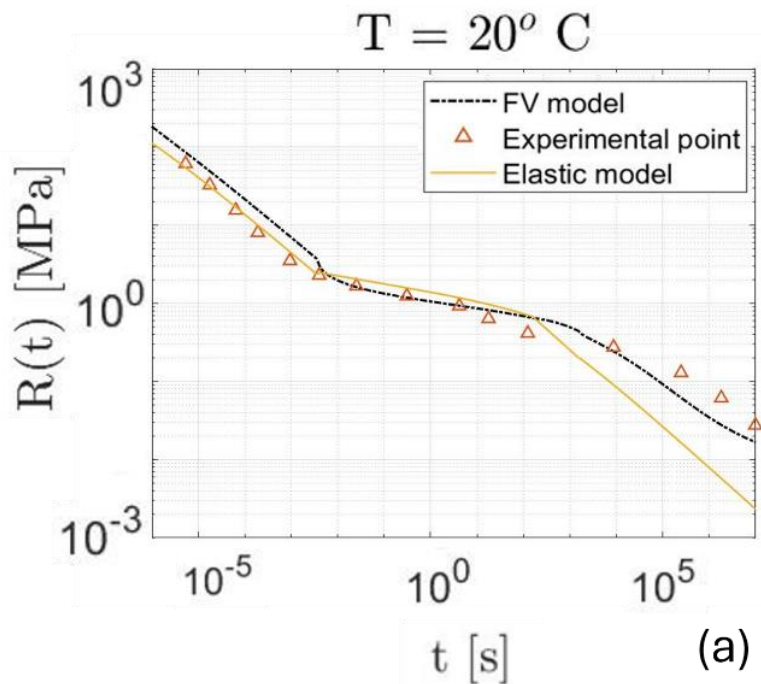


Model Results: Comparison with Elastic Model

Elastic Model

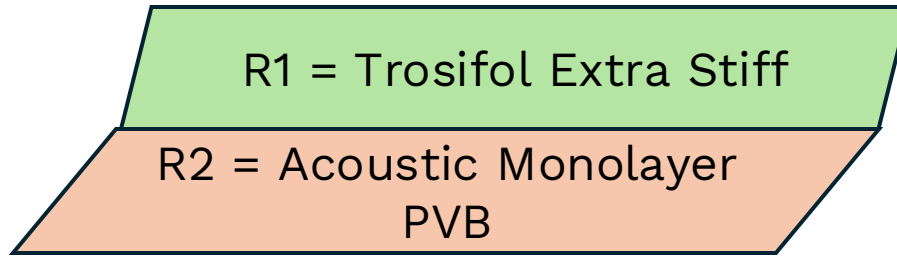
$$\frac{h_1+h_2}{R_m(t)} = \frac{h_1}{R_1(t)} + \frac{h_2}{R_2(t)}$$

Miriam Schuster · Michael Härth · Kerstin Thiele · Stephen J. Bennison. “Quantification of the linear viscoelastic behaviour of multilayer polymer interlayers for laminated glass”

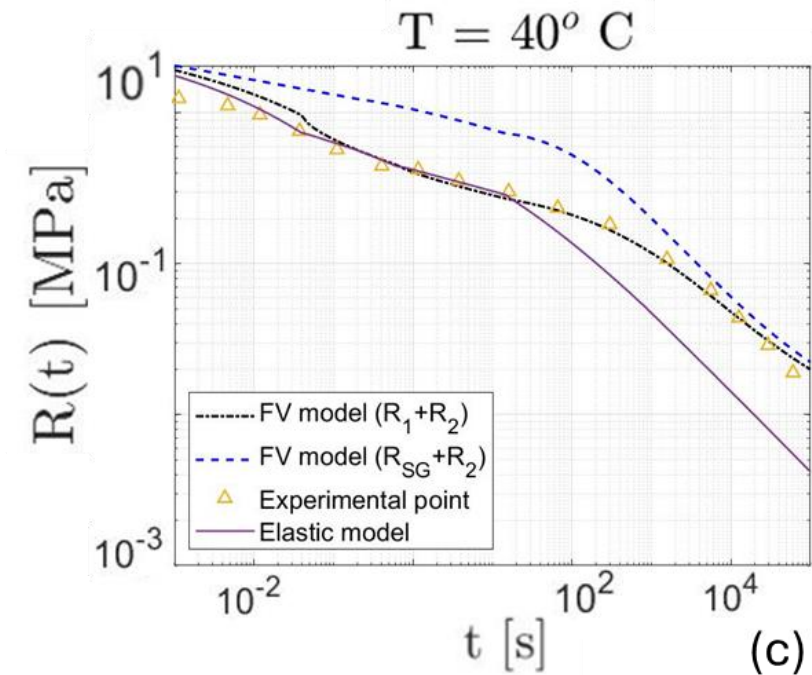
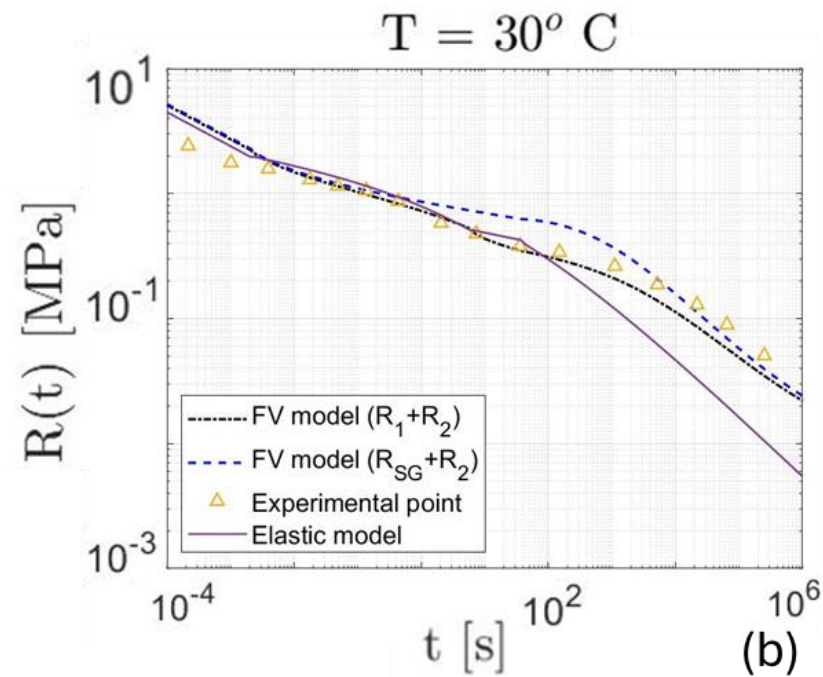
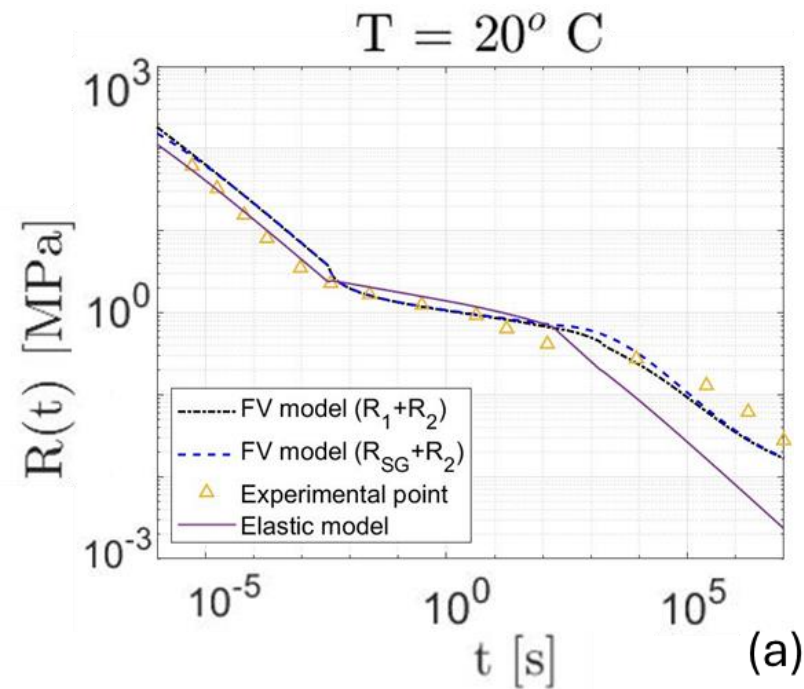
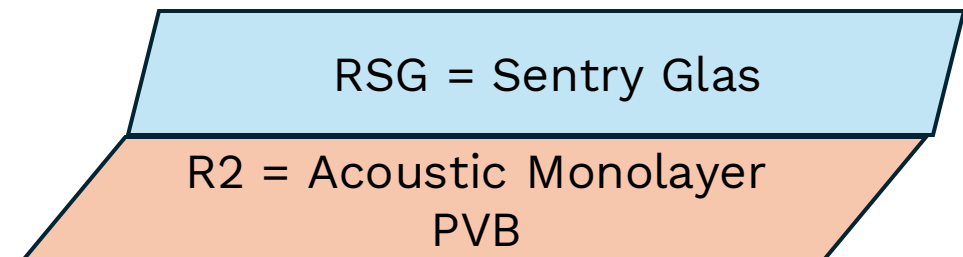


Optimization: Sentry Glas vs Trosifol Extra Stiff PRO

(a) - - - - -



(b) - - - - -



Conclusion

Methodology Validation

- Successfully applied power law interpolation to experimental relaxation data from DMTA analysis
- Implemented fractional derivatives to accurately characterize viscoelastic behavior

Model Performance

- The viscoelastic model demonstrates excellent agreement with experimental data
- Elastic models prove inadequate for reliable predictions

Practical Applications

- Method is generalizable to various MMPI configurations (different polymers, thicknesses)
- Enables predictive design of novel MMPI architectures

Industrial Relevance

- Provides reliable, interpretable mechanical response solutions

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Thank You

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